## Not Recommended for New Designs

The MAX495 was manufactured for Maxim by an outside wafer foundry using a process that is no longer available. It is not recommended for new designs. A Maxim replacement or an industry second-source may be available. The data sheet remains available for existing users. **The other parts on the following data sheet are not affected.** 

For further information, please see the QuickView data sheet for this part or contact <u>technical support</u> for assistance.

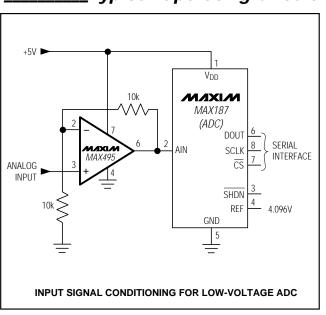
#### General Description

The dual MAX492, quad MAX494, and single MAX495 operational amplifiers combine excellent DC accuracy with rail-to-rail operation at the input and output. Since the common-mode voltage extends from VCC to VEE, the devices can operate from either a single supply (+2.7V to +6V) or split supplies (±1.35V to ±3V). Each op amp requires less than 150µA supply current. Even with this low current, the op amps are capable of driving a 1k $\Omega$  load, and the input referred voltage noise is only 25nV/√Hz. In addition, these op amps can drive loads in excess of 1nF.

The precision performance of the MAX492/MAX494/ MAX495, combined with their wide input and output dynamic range, low-voltage single-supply operation, and very low supply current, makes them an ideal choice for battery-operated equipment and other low-voltage applications. The MAX492/MAX494/MAX495 are available in DIP and SO packages in the industry-standard op-amp pin configurations. The MAX495 is also available in the smallest 8-pin SO: the µMAX package.

#### Applications

Portable Equipment Battery-Powered Instruments Data Acquisition Signal Conditioning Low-Voltage Applications



### Typical Operating Circuit

\_Features

- Low-Voltage Single-Supply Operation (+2.7V to +6V)
- Rail-to-Rail Input Common-Mode Voltage Range
- Rail-to-Rail Output Swing
- ✤ 500kHz Gain-Bandwidth Product
- Unity-Gain Stable
- 150µA Max Quiescent Current per Op Amp
- No Phase Reversal for Overdriven Inputs
- ♦ 200µV Offset Voltage
- High Voltage Gain (108dB)
- + High CMRR (90dB) and PSRR (110dB)
- + Drives 1kΩ Load
- Drives Large Capacitive Loads
- ♦ MAX495 Available in µMAX Package—8-Pin SO

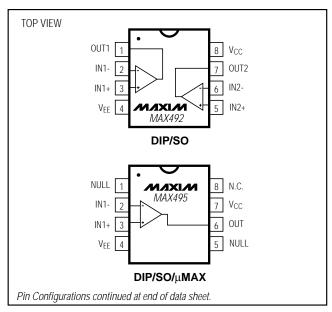
#### Ordering Information

PART	TEMP. RANGE	PIN-PACKAGE
MAX492CPA	0°C to +70°C	8 Plastic DIP
MAX492CSA	0°C to +70°C	8 SO
MAX492C/D	0°C to +70°C	Dice*
MAX492EPA	-40°C to +85°C	8 Plastic DIP
MAX492ESA	-40°C to +85°C	8 SO
MAX492MJA	-55°C to +125°C	8 CERDIP

Ordering Information continued at end of data sheet.

\*Dice are specified at TA = +25°C, DC parameters only.

#### Pin Configurations



#### 

Maxim Integrated Products 1

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#### ABSOLUTE MAXIMUM RATINGS

Supply Voltage (V <sub>CC</sub> to V <sub>EE</sub> )7V	14-Pin Plastic DIP (derate 10.00mW/°C above +70°C)800mW
Common-Mode Input Voltage(V <sub>CC</sub> + 0.3V) to (V <sub>EE</sub> - 0.3V)	14-Pin SO (derate 8.33mW/°C above +70°C)667mW
Differential Input Voltage±(V <sub>CC</sub> - V <sub>EE</sub> )	14-Pin CERDIP (derate 9.09mW/°C above +70°C)727mW
Input Current (IN+, IN-, NULL1, NULL2)±10mA	Operating Temperature Ranges
Output Short-Circuit DurationIndefinite short circuit	MAX49_C0°C to +70°C
to either supply	MAX49_E40°C to +85°C
Voltage Applied to NULL PinsVCC to VEE	MAX49_M55°C to +125°C
Continuous Power Dissipation ( $T_A = +70^{\circ}C$ )	Junction Temperatures
8-Pin Plastic DIP (derate 9.09mW/°C above +70°C)727mW	MAX49_C/E+150°C
8-Pin SO (derate 5.88mW/°C above +70°C)471mW	MAX49_M+175°C
8-Pin CERDIP (derate 8.00mW/°C above +70°C)640mW	Storage Temperature Range65°C to +150°C
8-Pin uMAX (derate 4.1mW/°C above +70°C)	Lead Temperature (soldering, 10sec)+300°C

Stresses beyond those listed under "Absolute Maximum Ratings" may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated in the operational sections of the specifications is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.

#### DC ELECTRICAL CHARACTERISTICS

(V<sub>CC</sub> = 2.7V to 6V, V<sub>EE</sub> = GND, V<sub>CM</sub> = 0V, V<sub>OUT</sub> = V<sub>CC</sub> / 2, T<sub>A</sub> = +25°C, unless otherwise noted.)

PARAMETER	COND	ITIONS	MIN	TYP	MAX	UNITS
Input Offset Voltage	$V_{CM} = V_{EE}$ to $V_{CC}$			±200	±500	μV
Input Bias Current	$V_{CM} = V_{EE}$ to $V_{CC}$			±25	±60	nA
Input Offset Current	VCM = VEE to VCC			±0.5	±6	nA
Differential Input Resistance				2		MΩ
Common-Mode Input Voltage Range			V <sub>EE</sub> - 0.25		V <sub>CC</sub> + 0.25	V
Common-Mode Rejection Ratio	$(V_{EE} - 0.25V) \le V_{CM} \le (V_{EE} - 0.25V)$	/cc + 0.25V)	74	90		dB
Power-Supply Rejection Ratio	$V_{CC} = 2.7V \text{ to } 6V$		88	110		dB
	$V_{CC} = 2.7V_{,}$	Sourcing	90	104		dB
	RL = 100kΩ, Vout = 0.25V to 2.45V	Sinking	90	102		
	$\label{eq:VC} \begin{array}{l} V_{CC} = 2.7 \text{V}, \ \text{R}_L = 1 \text{k} \Omega, \\ V_{OUT} = 0.5 \text{V} \ \text{to} \ 2.2 \text{V} \end{array}$	Sourcing	94	105		
Large-Signal Voltage Gain		Sinking	78	90		
(Note 1)	$V_{CC} = 5.0V,$ $R_L = 100k\Omega,$ $V_{OUT} = 0.25V \text{ to } 4.75V$	Sourcing	98	108		
		Sinking	92	100		
	$V_{CC} = 5.0V$ , $R_L = 1k\Omega$ ,	Sourcing	98	110		
	$V_{OUT} = 0.5V \text{ to } 4.5V$	Sinking	86	98		
	R <sub>L</sub> = 100k $\Omega$	V <sub>OH</sub>	V <sub>CC</sub> - 0.075	V <sub>CC</sub> - 0.04		
Output Voltage Swing		Vol		VEE + 0.04	VEE + 0.075	1
(Note 1)		V <sub>OH</sub>	V <sub>CC</sub> - 0.20	V <sub>CC</sub> - 0.15		V
	$R_L = 1k\Omega$	Vol		V <sub>EE</sub> + 0.15	$V_{EE} + 0.20$	
Output Short-Circuit Current				30		mA
Operating Supply Voltage Range			2.7		6.0	V
Supply Current (per amplifier)	V <sub>CM</sub> = V <sub>OUT</sub> = V <sub>CC</sub> / 2	$V_{CC} = 2.7V$		135	150	
Supply Current (per ampliner)	$v_{\rm CM} = v_{\rm OUI} = v_{\rm CC}/2$	$V_{CC} = 5V$		150	170	μA



#### **AC ELECTRICAL CHARACTERISTICS**

(V\_CC = 2.7V to 6V, V\_EE = GND, T\_A = +25°C, unless otherwise noted.)

PARAMETER	CONDITIONS	MIN	TYP	MAX	UNITS
Gain-Bandwidth Product	$R_L = 100k\Omega$ , $C_L = 100pF$		500		kHz
Phase Margin	$R_L = 100k\Omega$ , $C_L = 100pF$		60		degrees
Gain Margin	$R_L = 100k\Omega$ , $C_L = 100pF$		10		dB
Total Harmonic Distortion	$R_L = 10k\Omega$ , $C_L = 15pF$ , $V_{OUT} = 2V_{p-p}$ , $A_V = +1$ , $f = 1kHz$		0.003		%
Slew Rate	$R_L = 100k\Omega$ , $C_L = 15pF$		0.20		V/µs
Time	To 0.1%, 2V step		12		μs
Turn-On Time	$V_{CC} = 0V$ to 3V step, $V_{IN} = V_{CC} / 2$ , $A_V = +1$		5		μs
Input Noise-Voltage Density	f = 1kHz		25		nV/√Hz
Input Noise-Current Density	f = 1kHz		0.1		pA/√Hz
Amp-Amp Isolation	f = 1kHz		125		dB

#### DC ELECTRICAL CHARACTERISTICS

(V<sub>CC</sub> = 2.7V to 6V, V<sub>EE</sub> = GND, V<sub>CM</sub> = 0V, V<sub>OUT</sub> = V<sub>CC</sub> / 2, T<sub>A</sub> = 0°C to +70°C, unless otherwise noted.)

PARAMETER	CONDITIONS		MIN	TYP	MAX	UNITS	
Input Offset Voltage	$V_{CM} = V_{EE}$ to $V_{CC}$			±650	μV		
Input Offset Voltage Tempco			±2		μV/°C		
Input Bias Current	VCM = VEE to VCC				±75	nA	
Input Offset Current	$V_{CM} = V_{EE}$ to $V_{CC}$				±6	nA	
Common-Mode Input Voltage Range					C + 0.20	V	
Common-Mode Rejection Ratio	$(V_{EE} - 0.20) \le V_{CM} \le (V_{CC} + 0.20)$	- 0.20)	72			dB	
Power-Supply Rejection Ratio	Vcc = 2.7V to 6V		86			dB	
	$V_{CC} = 2.7 V, R_L = 100 k\Omega,$	Sourcing	88				
	V <sub>OUT</sub> = 0.25V to 2.45V	Sinking	84			dB	
	$\label{eq:VCC} \begin{array}{l} V_{CC} = 2.7 V, \ R_L = 1 k \Omega, \\ V_{OUT} = 0.5 V \ to \ 2.2 V \end{array}$	Sourcing	92				
Large-Signal Voltage Gain		Sinking	76				
(Note 1)	$\label{eq:VCC} \begin{array}{l} V_{CC} = 5.0V, \ R_L = 100 k \Omega, \\ V_{OUT} = 0.25V \ to \ 4.75V \end{array}$	Sourcing	92			uВ	
		Sinking	88				
	$V_{CC} = 5.0V, R_L = 1k\Omega,$	Sourcing	96				
	$V_{OUT} = 0.5V \text{ to } 4.5V$	Sinking	82				
	$R_{I} = 100 k \Omega$	V <sub>OH</sub>	V <sub>CC</sub> - 0.07	5			
Output Voltage Swing (Note 1)	KL = 100K22	Vol		VE	E + 0.075	V	
	$R_{I} = 1k\Omega$	VOH	V <sub>CC</sub> - 0.20			v	
	$N_{\rm L} = 1N_{\rm S2}$	VOL		V	EE + 0.20		
Operating Supply Voltage Range			2.7		6.0	V	
Supply Current (per amplifier)	$V_{CM} = V_{OUT} = V_{CC} / 2$	$V_{CC} = 2.7V$			175	μA	
Supply Current (per amplitier)		$V_{CC} = 5V$			190	μΑ	

#### DC ELECTRICAL CHARACTERISTICS

(V<sub>CC</sub> = 2.7V to 6V, V<sub>EE</sub> = GND, V<sub>CM</sub> = 0V, V<sub>OUT</sub> = V<sub>CC</sub> / 2, T<sub>A</sub> = -40°C to +85°C, unless otherwise noted.)

PARAMETER	CONE	DITIONS	MIN	ΤΥΡ	MAX	UNITS	
Input Offset Voltage	$V_{CM} = V_{EE}$ to $V_{CC}$			±950	μV		
Input Offset Voltage Tempco						µV/°C	
Input Bias Current	VCM = VEE to VCC				±100	nA	
Input Offset Current	$V_{CM} = V_{EE}$ to $V_{CC}$				±8	nA	
Common-Mode Input Voltage Range			V <sub>EE</sub> - 0.15	Vc	C + 0.15	V	
Common-Mode Rejection Ratio	(V <sub>EE</sub> - 0.15) ≤ V <sub>CM</sub> ≤ (V <sub>CC</sub> +	0.15)	68			dB	
Power-Supply Rejection Ratio	$V_{CC} = 2.7V$ to 6V, $V_{CM} = 0V$	/	84			dB	
	$V_{CC} = 2.7 V, R_{L} = 100 k \Omega,$	Sourcing	86				
	V <sub>OUT</sub> = 0.25V to 2.45V	Sinking	84			- dB	
	$\label{eq:VCC} \begin{array}{l} V_{CC} = 2.7 \text{V}, \ \text{R}_{\text{L}} = 1 \text{k} \Omega, \\ V_{OUT} = 0.5 \text{V} \ \text{to} \ 2.2 \text{V} \end{array}$	Sourcing	92				
Large-Signal Voltage Gain (Note 1)		Sinking	76				
	$\label{eq:VCC} \begin{array}{l} V_{CC} = 5.0 V, \ R_L = 100 k \Omega, \\ V_{OUT} = 0.25 V \ to \ 4.75 V \end{array}$	Sourcing	92				
		Sinking	86				
	$V_{CC} = 5.0V, R_L = 1k\Omega,$	Sourcing	96				
	Vout = 0.5V to 4.5V	Sinking	80				
	$R_L = 100k\Omega$	Voh	Vcc - 0.07	5			
Output Voltage Swing		Vol		VEI	E + 0.075	V	
(Note 1)	D 110	VOH	V <sub>CC</sub> - 0.20			V	
	$R_L = 1k\Omega$	Vol		V	EE + 0.20		
Operating Supply-Voltage Range			2.7		6.0	V	
Supply Current (per amplifier)		$V_{CC} = 2.7V$			185		
Supply Current (per amplifier)	VCM = VOUT = VCC / 2	$V_{CC} = 5V$			200	μA	

#### DC ELECTRICAL CHARACTERISTICS

(V<sub>CC</sub> = 2.7V to 6V, V<sub>EE</sub> = GND, V<sub>CM</sub> = 0V, V<sub>OUT</sub> = V<sub>CC</sub> / 2, T<sub>A</sub> = -55°C to +125°C, unless otherwise noted.)

PARAMETER	CONDI	MIN	TYP	MAX	UNITS	
Input Offset Voltage	VCM = VEE to VCC			±1.2	mV	
Input Offset Voltage Tempco				±2		µV/°C
Input Bias Current	VCM = VEE to VCC				±200	nA
Input Offset Current	$V_{CM} = V_{EE}$ to $V_{CC}$				±10	nA
Common-Mode Input Voltage Range			V <sub>EE</sub> - 0.05	VC	C + 0.05	V
Common-Mode Rejection Ratio	$(V_{EE} - 0.05V) \le V_{CM} \le (V_{CC})$	+ 0.05V)	66			dB
Power-Supply Rejection Ratio	$V_{CC} = 2.7 V$ to 6V		80			dB
	$V_{CC} = 2.7 V, R_{L} = 100 k\Omega,$	Sourcing	82			
	V <sub>OUT</sub> = 0.25V to 2.45V	Sinking	80			ĺ
	$\label{eq:VCC} \begin{array}{l} V_{CC} = 2.7 V, \ R_L = 1 k \Omega, \\ V_{OUT} = 0.5 V \ to \ 2.2 V \end{array}$	Sourcing	90			
Large-Signal Voltage Gain		Sinking	72			dB
(Note 1)	$\label{eq:VCC} \begin{array}{l} V_{CC} = 5.0V, \ R_L = 100 k \Omega, \\ V_{OUT} = 0.25V \ to \ 4.75V \end{array}$	Sourcing	86			
		Sinking	82			
	$V_{CC} = 5.0V$ , $R_L = 1k\Omega$ ,	Sourcing	94			
	VOUT = 0.5V to 4.5V	Sinking	76			
	$R_{I} = 100 k \Omega$	Voh	Vcc - 0.07	5		
Output Voltage Swing	RL = 100K22	Vol		VEE	+ 0.075	V
(Note 1)	D: 11/0	V <sub>OH</sub>	V <sub>CC</sub> - 0.25	0		V
	$R_L = 1k\Omega$	Vol		VEE	+ 0.250	
Operating Supply-Voltage Range			2.7		6.0	V
Supply Current (per amplifier)	New New New 12	$V_{CC} = 2.7V$			200	
Supply Current (per amplifier)	$V_{CM} = V_{OUT} = V_{CC} / 2$	$V_{CC} = 5V$			225	μA

Note 1: RL to VEE for sourcing and VOH tests; RL to VCC for sinking and VOL tests.

160

140

₹<sup>120</sup>

100

80

60

40

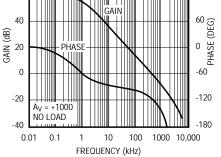
20

0

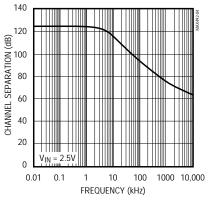
OFFSET VOLTAGE

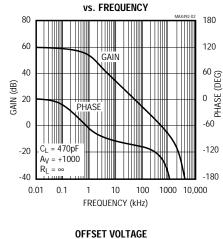
INPUT BIAS CURRENT (nA)

(T<sub>A</sub> = +25°C, V<sub>CC</sub> = 5V, V<sub>EE</sub> = 0V, unless otherwise noted.) GAIN AND PHASE vs. FREQUENCY 120 60120 60









vs. TEMPERATURE

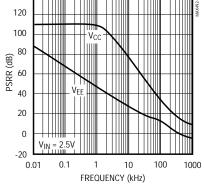
 $V_{CM} = 0V$ 

GAIN AND PHASE

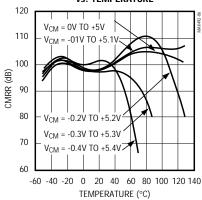
#### **Typical Operating Characteristics**

140

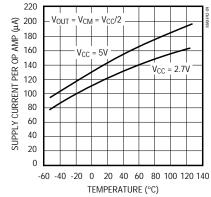
POWER-SUPPLY REJECTION RATIO vs. FREQUENCY

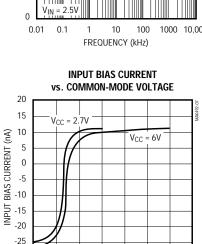


COMMON-MODE REJECTION RATIO vs. TEMPERATURE

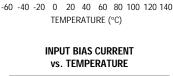


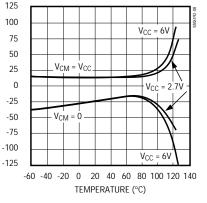
SUPPLY CURRENT PER AMPLIFIER vs. TEMPERATURE





 $V_{CM}$  (V)





6

-30

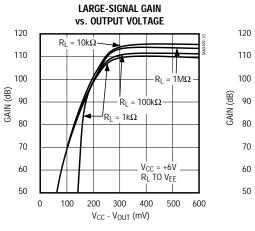
0 1 2 3 4 5 6 7

MAX492/MAX494/MAX495

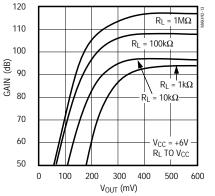
#### Typical Operating Characteristics (continued)

-ARGE-SIGNAL GAIN

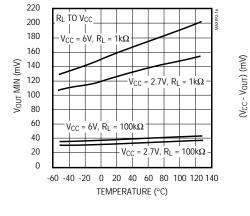
 $(T_A = +25^{\circ}C, V_{CC} = 5V, V_{EE} = 0V, unless otherwise noted.)$ 



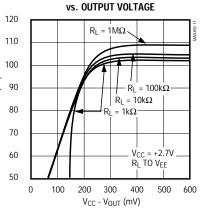








MIXIM



LARGE-SIGNAL GAIN

vs. OUTPUT VOLTAGE

 $R_L = 1k\Omega$ 

 $V_{CC} = +2.7V$ R<sub>L</sub> TO V<sub>CC</sub>

500 600

R = 10kΩ

Rı = 1MO

 $R_L = 100k\Omega$ 

100 200

120

110

100

90

80

70

60

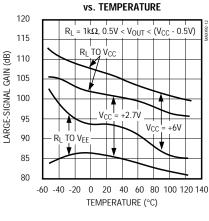
50

0

(qB)

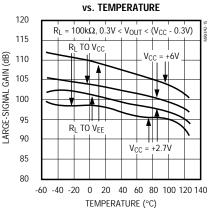
GAIN

LARGE-SIGNAL GAIN



LARGE-SIGNAL GAIN

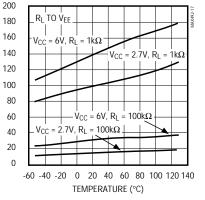
LARGE-SIGNAL GAIN



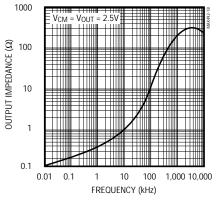
#### MAXIMUM OUTPUT VOLTAGE vs. TEMPERATURE

300 400

V<sub>OUT</sub> (mV)





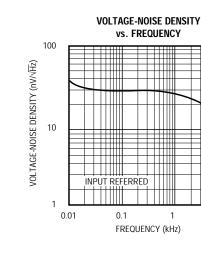




10

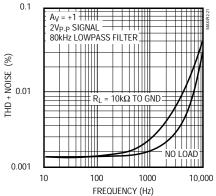
#### Typical Operating Characteristics (continued)

 $(T_A = +25^{\circ}C, V_{CC} = 5V, V_{EE} = 0V, unless otherwise noted.)$ 

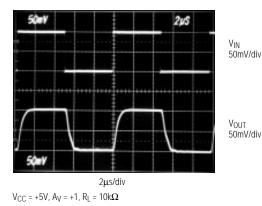


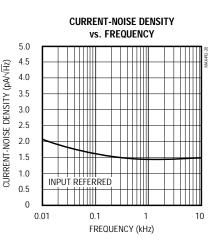
**TOTAL HARMONIC DISTORTION + NOISE** vs. FREQUENCY

1

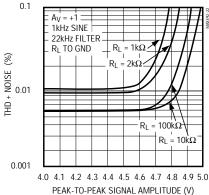


SMALL-SIGNAL TRANSIENT RESPONSE

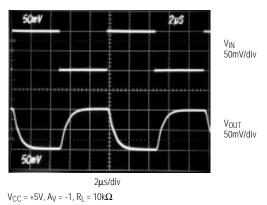




**TOTAL HARMONIC DISTORTION + NOISE** vs. PEAK-TO-PEAK SIGNAL AMPLITUDE



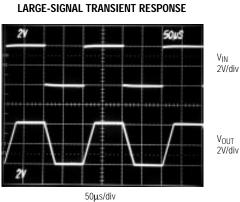
SMALL-SIGNAL TRANSIENT RESPONSE



MIXIM

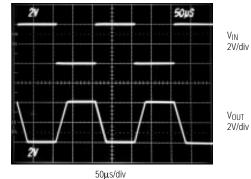
#### Typical Operating Characteristics (continued)

 $(T_A = +25^{\circ}C, V_{CC} = 5V, V_{EE} = 0V, unless otherwise noted.)$ 



 $V_{CC} = +5V, A_V = +1, R_L = 10k\Omega$ 

#### LARGE-SIGNAL TRANSIENT RESPONSE



 $V_{CC} = +5V, A_V = -1, R_L = 10k\Omega$ 

#### Pin Description

PIN		PIN		I NAME		FUNCTION
MAX492	MAX494	MAX495	NAME	FUNCTION		
1	1	—	OUT1	Amplifier 1 Output		
	_	1, 5	NULL	Offset Null Input. Connect to a 10k $\Omega$ potentiometer for offset-voltage trimming. Connect wiper to V <sub>EE</sub> (Figure 3).		
	—	2	IN-	Inverting Input		
2	2	—	IN1-	Amplifier 1 Inverting Input		
_	_	3	IN+	Noninverting Input		
3	3	—	IN1+	Amplifier 1 Noninverting Input		
4	11	4	VEE	Negative Power-Supply Pin. Connect to ground or a negative voltage.		
5	5	—	IN2+	Amplifier 2 Noninverting Input		
_	—	6	OUT	Amplifier Output		
6	6	—	IN2-	Amplifier 2 Inverting Input		
7	7	—	OUT2	Amplifier 2 Output		
8	4	7	Vcc	Positive Power-Supply Pin. Connect to (+) terminal of power supply.		
_	8	—	OUT3	Amplifier 3 Output		
—	9	—	IN3-	Amplifier 3 Inverting Input		
	10	—	IN3+	Amplifier 3 Noninverting Input		
	12	_	IN4+	Amplifier 4 Noninverting Input		
	13	—	IN4-	Amplifier 4 Inverting Input		
	14	—	OUT4	Amplifier 4 Output		
—	_	8	N.C.	No Connect. Not internally connected.		

#### 

# MAX492/MAX494/MAX495

#### \_Applications Information

The dual MAX492, quad MAX494, and single MAX495 op amps combine excellent DC accuracy with rail-torail operation at both input and output. With their precision performance, wide dynamic range at low supply voltages, and very low supply current, these op amps are ideal for battery-operated equipment and other lowvoltage applications.

#### **Rail-to-Rail Inputs and Outputs**

The MAX492/MAX494/MAX495's input common-mode range extends 0.25V **beyond** the positive and negative supply rails, with excellent common-mode rejection. Beyond the specified common-mode range, the outputs are guaranteed not to undergo phase reversal or latchup. Therefore, the MAX492/MAX494/MAX495 can be used in applications with common-mode signals at or even beyond the supplies, without the problems associated with typical op amps.

The MAX492/MAX494/MAX495's output voltage swings to within 50mV of the supplies with a 100k $\Omega$  load. This rail-to-rail swing at the input and output substantially increases the dynamic range, especially in low supply-voltage applications. Figure 1 shows the input and output waveforms for the MAX492, configured as a unity-gain noninverting buffer operating from a single +3V supply. The input signal is 3.0Vp-p, 1kHz sinusoid centered at +1.5V. The output amplitude is approximately 2.95Vp-p.

#### Input Offset Voltage

Rail-to-rail common-mode swing at the input is obtained by two complementary input stages in parallel, which feed a folded cascaded stage. The PNP stage is active for input voltages close to the negative rail, and the NPN stage is active for input voltages close to the positive rail.

The offsets of the two pairs are trimmed; however, there is some small residual mismatch between them. This mismatch results in a two-level input offset characteristic, with a transition region between the levels occurring at a common-mode voltage of approximately 1.3V. Unlike other rail-to-rail op amps, the transition region has been widened to approximately 600mV in order to minimize the slight degradation in CMRR caused by this mismatch.

To adjust the MAX495's input offset voltage (500µV max at +25°C), connect a 10k $\Omega$  trim potentiometer between the two NULL pins (pins 1 and 5), with the wiper connected to VEE (pin 4) (Figure 2). The trim range of this circuit is ±6mV. External offset adjustment is not available for the dual MAX492 or quad MAX494.

The input bias currents of the MAX492/MAX494/MAX495 are typically less than 50nA. The bias current flows into the device when the NPN input stage is active, and it flows out when the PNP input stage is active. To reduce the offset error caused by input bias current flowing through external source resistances, match the effective resistance seen at each input. Connect resistor R3 between the noninverting input and ground when using

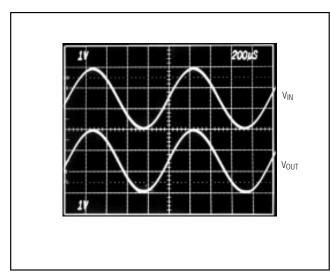


Figure 1. Rail-to-Rail Input and Output (Voltage Follower Circuit,  $V_{CC} = +3V$ ,  $V_{EE} = 0V$ )

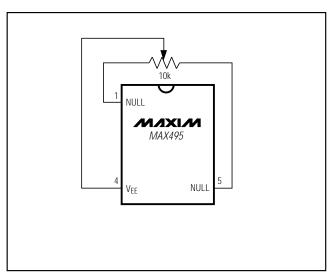


Figure 2. Offset Null Circuit



the op amp in an inverting configuration (Figure 3a); connect resistor R3 between the noninverting input and the input signal when using the op amp in a noninverting configuration (Figure 3b). Select R3 to equal the parallel combination of R1 and R2. High source resistances will degrade noise performance, due to the thermal noise of the resistor and the input current noise (which is multiplied by the source resistance).

#### Input Stage Protection Circuitry

The MAX492/MAX494/MAX495 include internal protection circuitry that prevents damage to the precision input stage from large differential input voltages. This protection circuitry consists of back-to-back diodes between IN+ and IN- with two  $1.7k\Omega$  resistors in series

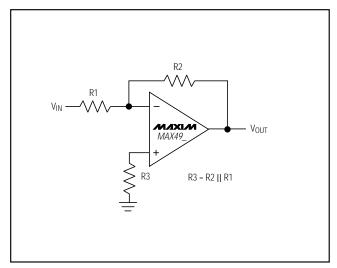


Figure 3a. Reducing Offset Error Due to Bias Current: Inverting Configuration

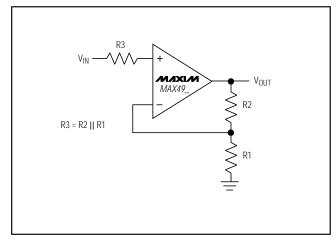


Figure 3b. Reducing Offset Error Due to Bias Current: Noninverting Configuration

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(Figure 4). The diodes limit the differential voltage applied to the amplifiers' internal circuitry to no more than  $V_F$ , where  $V_F$  is the diodes' forward-voltage drop (about 0.7V at +25°C).

Input bias current for the ICs ( $\pm 25nA$  typical) is specified for the small differential input voltages. For large differential input voltages (exceeding V<sub>F</sub>), this protection circuitry increases the input current at IN+ and IN-:

Input Current =  $\frac{(V_{IN} + V_{IN}) - V_F}{2 \times 1.7 k\Omega}$ 

For comparator applications requiring large differential voltages (greater than  $V_F$ ), you can limit the input current that flows through the diodes with external resistors

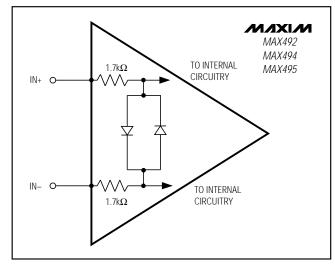


Figure 4. Input Stage Protection Circuitry

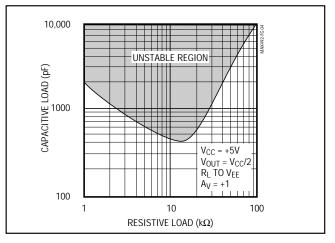


Figure 5. Capacitive-Load Stable Region Sourcing Current

in series with IN-, IN+, or both. Series resistors are not recommended for amplifier applications, as they may increase input offsets and decrease amplifier bandwidth.

#### **Output Loading and Stability**

Even with their low quiescent current of less than 150µÅ per op amp, the MAX492/MAX494/MAX495 are well suited for driving loads up to  $1k\Omega$  while maintaining DC accuracy. Stability while driving heavy capacitive loads is another key advantage over comparable CMOS rail-to-rail op amps.

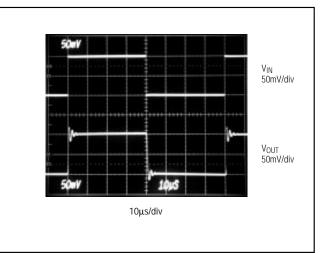


Figure 6. MAX492 Voltage Follower with 1000pF Load  $(R_L = \infty)$ 

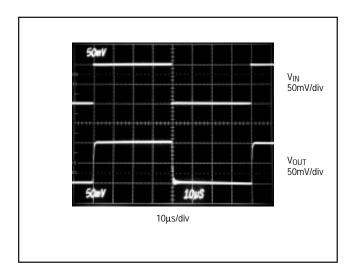


Figure 7a. MAX492 Voltage Follower with 500pF Load—  $R_L = 5k\Omega$ 

In op amp circuits, driving large capacitive loads increases the likelihood of oscillation. This is especially true for circuits with high loop gains, such as a unitygain voltage follower. The output impedance and a capacitive load form an RC network that adds a pole to the loop response and induces phase lag. If the pole frequency is low enough—as when driving a large capacitive load—the circuit phase margin is degraded, leading to either an under-damped pulse response or oscillation.

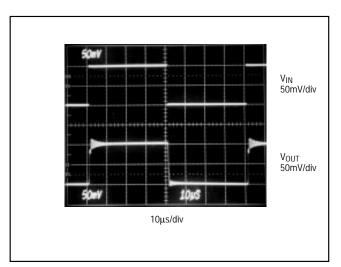


Figure 7b. MAX492 Voltage Follower with 500pF Load—  $R_L = 20k\Omega$ 

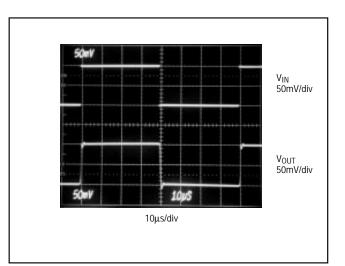


Figure 7c. MAX492 Voltage Follower with 500pF Load— $R_L = \infty$ 



The MAX492/MAX494/MAX495 can drive capacitive loads in excess of 1000pF under certain conditions (Figure 5). When driving capacitive loads, the greatest potential for instability occurs when the op amp is sourcing approximately 100µA. Even in this case, stability is maintained with up to 400pF of output capacitance. If the output sources either more or less current, stability is increased. These devices perform well with a 1000pF pure capacitive load (Figure 6). Figure 7 shows the performance with a 500pF load in parallel with various load resistors.

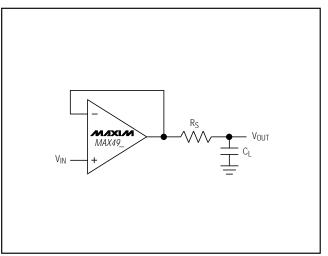


Figure 8. Capacitive-Load Driving Circuit

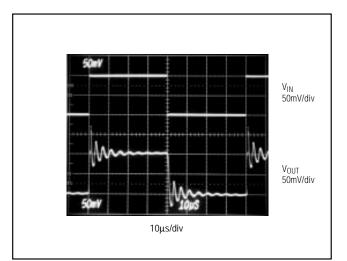


Figure 9a. Driving a 10,000pF Capacitive Load

To increase stability while driving large capacitive loads, connect a pull-up resistor at the output to decrease the current that the amplifier must source. If the amplifier is made to sink current rather than source, stability is further increased.

Frequency stability can be improved by adding an output isolation resistor (Rs) to the voltage-follower circuit (Figure 8). This resistor improves the phase margin of the circuit by isolating the load capacitor from the op amp's output. Figure 9a shows the MAX492 driving 10,000pF (RL  $\geq$  100k $\Omega$ ), while Figure 9b adds a 47 $\Omega$  isolation resistor.

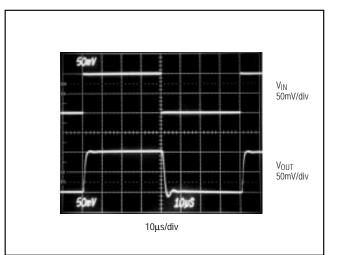


Figure 9b. Driving a 10,000pF Capacitive Load with a  $47\Omega$  Isolation Resistor

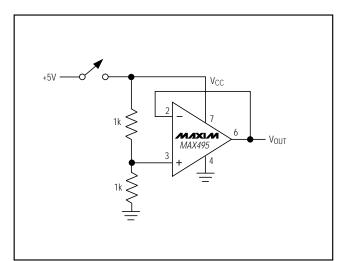


Figure 10. Power-Up Test Configuration

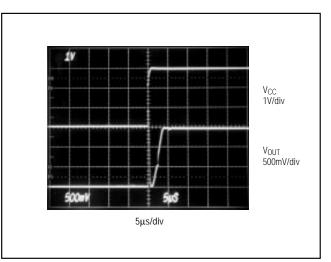


Figure 11a. Power-Up Settling Time ( $V_{CC} = +3V$ )

Because the MAX492/MAX494/MAX495 have excellent stability, no isolation resistor is required, except in the most demanding applications. This is beneficial because an isolation resistor would degrade the lowfrequency performance of the circuit.

#### **Power-Up Settling Time**

The MAX492/MAX494/MAX495 have a typical supply current of 150µA per op amp. Although supply current is already low, it is sometimes desirable to reduce it further by powering down the op amp and associated ICs for periods of time. For example, when using a MAX494 to buffer the inputs to a multi-channel analog-to-digital converter (ADC), much of the circuitry could be powered down between data samples to increase battery life. If samples are taken infrequently, the op amps, along with the ADC, may be powered down most of the time.

When power is reapplied to the MAX492/MAX494/ MAX495, it takes some time for the voltages on the supply pin and the output pin of the op amp to settle. Supply settling time depends on the supply voltage, the value of the bypass capacitor, the output impedance of the incoming supply, and any lead resistance or inductance between components. Op amp settling time depends primarily on the output voltage and is slew-rate limited. With the noninverting input to a voltage follower held at mid-supply (Figure 10), when the supply steps from OV to V<sub>CC</sub>, the output settles in approximately 4 $\mu$ s for V<sub>CC</sub> = +3V (Figure 11a) or 10 $\mu$ s for V<sub>CC</sub> = +5V (Figure 11b).

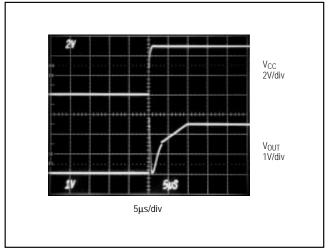


Figure 11b. Power-Up Settling Time ( $V_{CC} = +5V$ )

#### **Power Supplies and Layout**

The MAX492/MAX494/MAX495 operate from a single 2.7V to 6V power supply, or from dual supplies of  $\pm 1.35V$  to  $\pm 3V$ . For single-supply operation, bypass the power supply with a 1µF capacitor in parallel with a 0.1µF ceramic capacitor. If operating from dual supplies, bypass each supply to ground.

Good layout improves performance by decreasing the amount of stray capacitance at the op amp's inputs and output. To decrease stray capacitance, minimize both trace lengths and resistor leads and place external components close to the op amp's pins.

#### Rail-to-Rail Buffers

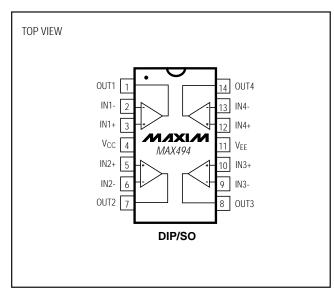
The *Typical Operating Circuit* shows a MAX495 gain-oftwo buffer driving the analog input to a MAX187 12-bit ADC. Both devices run from a single 5V supply, and the converter's internal reference is 4.096V. The MAX495's typical input offset voltage is  $200\mu$ V. This results in an error at the ADC input of  $400\mu$ V, or less than half of one least significant bit (LSB). Without offset trimming, the op amp contributes negligible error to the conversion result.

PART	TEMP. RANGE	PIN-PACKAGE
MAX494CPD	0°C to +70°C	14 Plastic DIP
MAX494CSD	0°C to +70°C	14 SO
MAX494EPD	-40°C to +85°C	14 Plastic DIP
MAX494ESD	-40°C to +85°C	14 SO
MAX494MJD	-55°C to +125°C	14 CERDIP
MAX495CPA	0°C to +70°C	8 Plastic DIP
MAX495CSA	0°C to +70°C	8 SO
MAX495CUA	0°C to +70°C	8 µMAX
MAX495C/D	0°C to +70°C	Dice*
MAX495EPA	-40°C to +85°C	8 Plastic DIP
MAX495ESA	-40°C to +85°C	8 SO
MAX495MJA	-55°C to +125°C	8 CERDIP

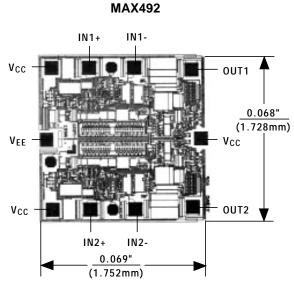
#### \_Ordering Information (continued)

\* Dice are specified at  $T_A = +25$  °C, DC parameters only.

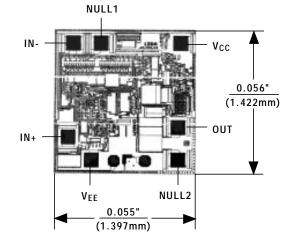
#### Pin Configurations (continued)



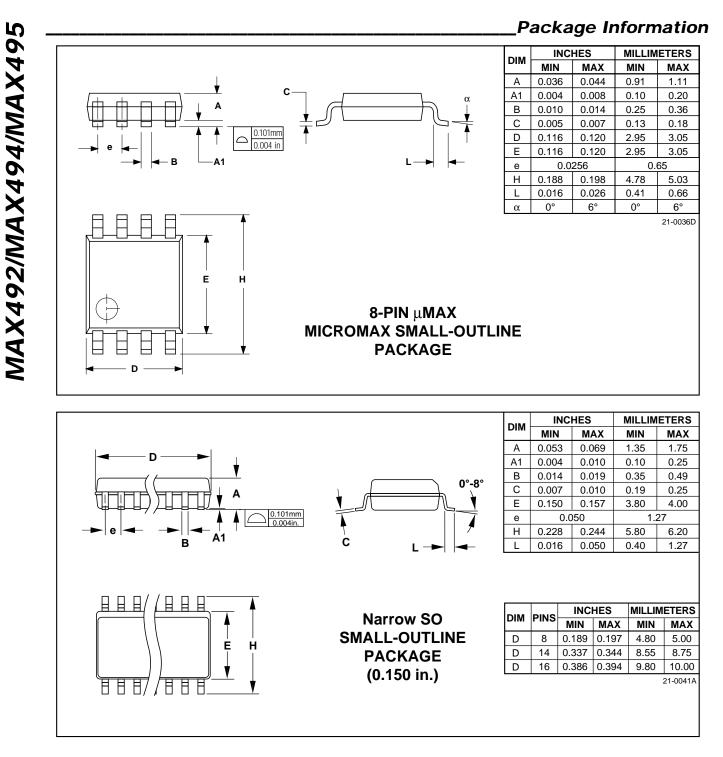
#### \_\_\_Chip Topographies



MAX495



TRANSISTOR COUNT: 134 (single MAX495) 268 (dual MAX492) 536 (quad MAX494) SUBSTRATE CONNECTED TO VFF



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